

Key Equations:

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$$(V_{IC})_{max} = V_{DD} - V_{OV3} - V_{E3} + V_{E1}$$

$$(V_{IC})_{min} = V_{OV5} + V_{OV1} + V_{E1}$$

$$(V_O)_{max} = V_{DD} - V_{OV6} ; (V_O)_{min} = V_{OV7}$$

$$V_{OV6} = V_{OV3} = V_{OV4}$$

$$SR_{C_{gdb}} = \frac{I_{B1}}{C_{gdb}} ; SR_{C_L}^- = \frac{I_{B2}}{C_L}$$

$$SR_{C_L}^+ = \frac{I_{O6-max} - I_{B2}}{C_L}$$

$$A_0 = G_{m1} R_1 G_{m2} R_2$$

$$f_{p1} = \frac{1}{2\pi (R_1 C_1 + R_2 C_2 + (R_1 + R_2 + G_{m2} R_1 R_2) C_{gdb})}$$

where: $G_{m1} = g_{m1,2}$, $R_1 = r_{ds4} // r_{ds2}$

$$G_{m2} = g_{m6} , R_2 = R_{out} = r_{ds6} // r_{ds7}$$

C_1 = all caps @ V_4 to small-signal gnd

C_2 = all caps @ V_O to ss gnd (incl. C_L)

$$f_{p1} \approx \frac{1}{2\pi G_{m2} R_1 R_2 C_{gdb}}$$

• Unity-gain freq = $G \cdot BW = \frac{G_{m1}}{2\pi C_{gd6}}$

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• Design Procedure:

- Select bias currents I_{B1} & I_{B2}

• Meet SR requirements, power limitations, size constraints.

- $G \cdot BW \Rightarrow G_{m1} \Rightarrow (\omega/L)_{1,2}$

- $ICMR \Rightarrow (\omega/L)_{3,4}$ & $(\omega/L)_5$

- (V_o) Range $\Rightarrow (\omega/L)_6$ & $(\omega/L)_7$

- $V_{ov3} = V_{ov6} \Rightarrow (\omega/L)_6$

- $A_o \Rightarrow G_{m2}$ & R_1 & $R_2 \Rightarrow (\omega/L)_6, L_7, L_6, L_4, L_2$

\Rightarrow At this point, we have more degrees of

freedom than constraints.

\Rightarrow analyze feedback & stability

\Rightarrow additional constraints.