

$$\textcircled{1} \text{ a) } I_{OUT} = \frac{V_{BE}}{R} = I_S e^{V_{BE}/V_T}$$

→ need numerical solver, since I_{OUT} appears inside & outside exp

$$0 = \frac{V_{BE}}{R} - I_S e^{V_{BE}/V_T} = \frac{V_{BE}}{10^3} - 10^{-15} e^{V_{BE}/26 \cdot 10^{-3}}$$

⇒ using MATLAB function "fzero" ⇒ $V_{BE}|_{T=T_0} = 647.2 \text{ mV} = V_{BE0}$

T	$V_{BE} = V_{BE0} - \Delta T \cdot 1.8 \text{ mV}/^\circ\text{C}$	$R = R_0 + \Delta T \cdot 15 \Omega/^\circ\text{C}$	$I_{OUT} = \frac{V_{BE}}{R} //$
27°C	647.2 mV	10 kΩ	64.72 μA
0°C	695.8 mV	9.595 kΩ	72.52 μA
100°C	515.8 mV	11.095 kΩ	46.49 μA

b) plot I_{OUT} vs. TEMP → see attached
 PSPICE input file → see attached
 Comparison hand analysis vs. simulation:

T	I_{OUT} calculated	I_{OUT} simulated	error = $\frac{\text{sim} - \text{calc}}{\text{sim}} \cdot 100\%$
27°C	64.72 μA	64.4 μA	-0.5%
0°C	72.52 μA	72.4 μA	-0.2%
100°C	46.49 μA	44.9 μA	-3.5%*

* this relatively large error results from an assumption we made in a). In the hand analysis, we are assuming a constant TC of $-1.8 \text{ mV}/^\circ\text{C}$. However, since I_{OUT} is decreasing, V_{BE} also changes due to this decrease in current, which results in a slightly larger overall temperature dependence!

c) Max. deviation occurs at 100°C: $\frac{64.4 - 44.9}{64.4} = \underline{\underline{30.3\%}}$
 (simulated data)

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a) $V_{out} = V_{BE1} + 2I \cdot R_1 = V_{BE1} + \frac{R_1}{R_2} \cdot 2V_T \ln 10$

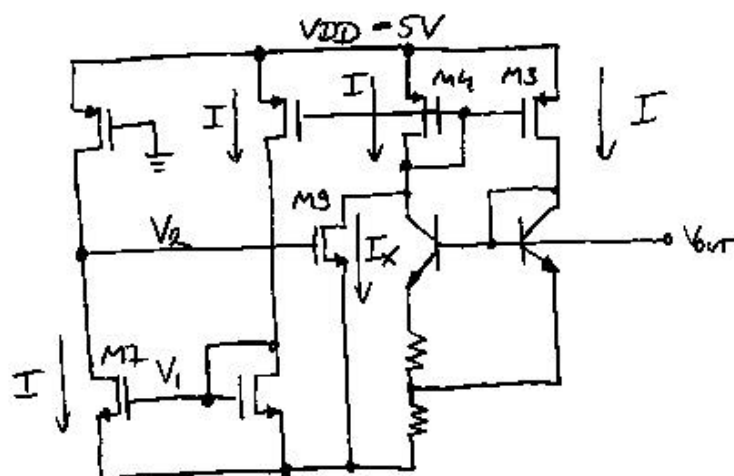
$$\frac{dV_{out}}{dT} = \frac{dV_{BE}}{dT} + \frac{R_1}{R_2} \cdot 2 \frac{k}{q} \ln 10 \stackrel{!}{=} 0$$

$$\Rightarrow \frac{R_1}{R_2} = - \frac{dV_{BE}}{dT} \cdot \frac{q}{2k \ln 10} = +1.8 \frac{mV}{^\circ C} \cdot \frac{1.6 \cdot 10^{-19} As}{2 \cdot 1.38 \cdot 10^{-23} J/^\circ C \ln 10}$$

$$\Rightarrow \frac{R_1}{R_2} = \underline{\underline{4.53}}$$

b) $I = \frac{V_T}{R_2} \ln 10 \Rightarrow R_2 = \frac{V_T}{I} \ln 10 = \frac{26mV}{10\mu A} \cdot \ln 10 = \underline{\underline{5.99 k\Omega}}$

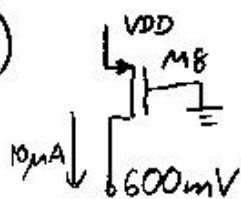
c)



	I	V ₁	V ₂	I _x
Before Startup:	0	0	V _{DD}	≠ 0
After Startup:	10μA	V _{TH} + V _{DD}	< 0.6V	0

In the possible bias point where $I=0$, $V_2 = V_{DD}$, which turns on M9. M9 then forces a current through M3/M4 which starts up the circuit. After startup, M9 turns off again, since M7 pulls down the gate of M9 to a voltage $< V_{TH}$.

d)



→ M8 is in SAT since $V_{DS} = (V_{DD} - 0.6V) > (V_{GS} - V_T) = V_{DD} - 1V$

$$\Rightarrow I = \frac{1}{2} \mu_p \frac{W}{L} (V_{DD} - V_{TH})^2$$

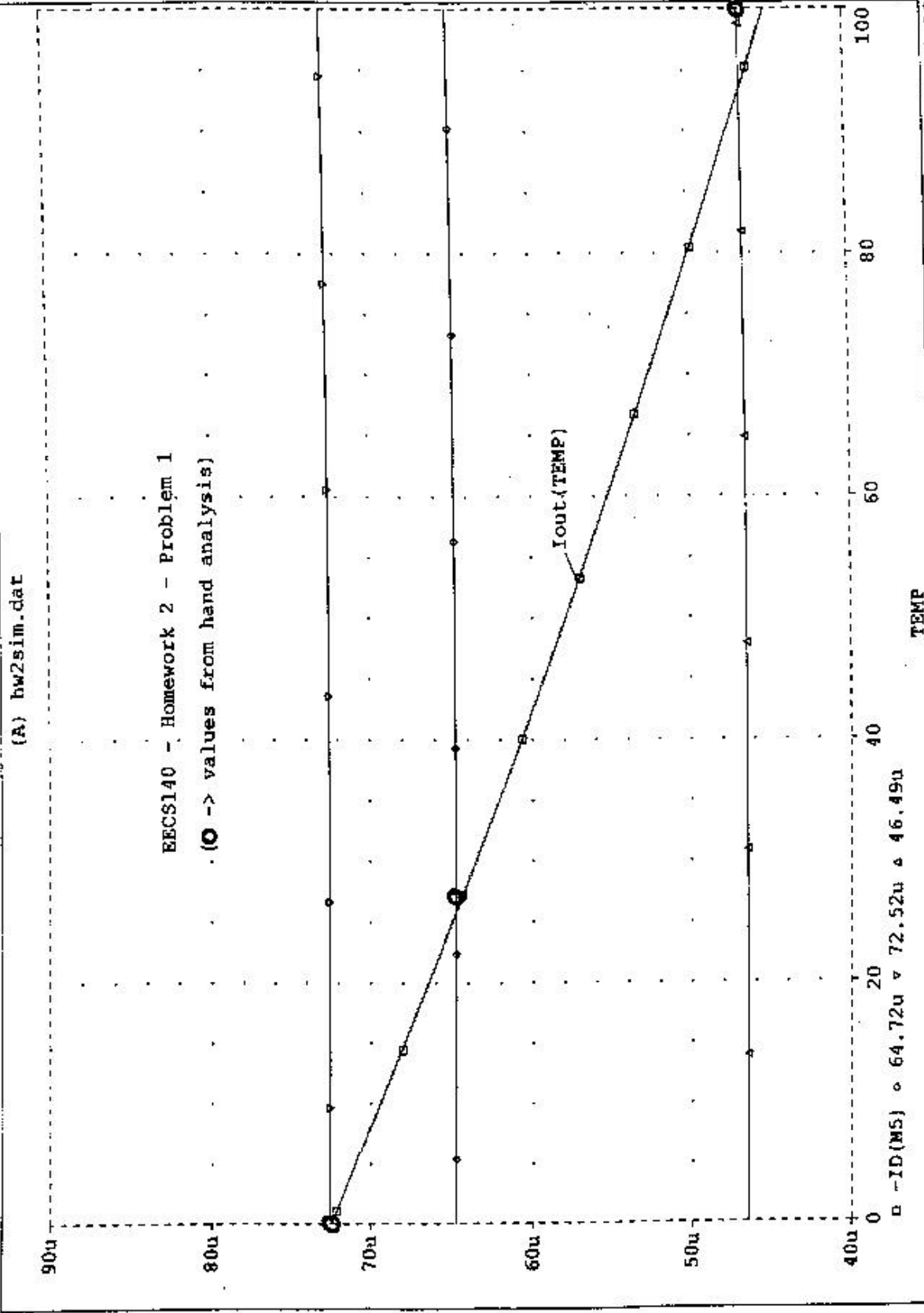
$$\frac{W}{L} \leq \frac{2I}{\mu_p (V_{DD} - V_{TH})^2} = \frac{2 \cdot 10\mu A}{100 \frac{A}{V^2} \cdot (5-1)^2 V^2} = \underline{\underline{\frac{1}{80}}}$$

So $(\frac{W}{L})_8$ needs to be less than $\frac{1}{80}$. //

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Temperature: 0.0

Date/time run: 08/29/99 21:21:36



Time: 21:41:18

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Date: August 29, 1999

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*** EECS140 - Homework 2 - Problem 1
*** Example Spice Deck for PSPICE, looks quite similar for HSpice...
*** Boris Murmann, FALL '99

** Analysis setup **

```
.DC LIN TEMP 0 100 0.1  
options stepgmin  
.probe
```

** Schematics Netlist **

```
V_VDD      vdd 0 10  
Q_Q1      1 vb 0 NPNi  
M_M3      1 vbp vdd vdd PMOSi  
+ L=2u  
+ W=50u  
M_M4      vbp vbp vdd vdd PMOSi  
+ L=2u  
+ W=50u  
M_M5      0 vbp vdd vdd PMOSi  
+ L=2u  
+ W=50u  
M_M2      vbp 1 vb vb NMOSi  
+ L=2u  
+ W=50u  
R_R5      0 vb 10k TC1=1.5m
```

** (idealized) Models **

```
.model npni npn is=1f bf=1E6 va=1000 tf=20p  
.model nmosi nmos vto=1 tox=6.9n kp=200u lambda=0 gamma=0.5 phi=0.6  
.model pmosi pmos vto=-1 tox=6.9n kp=100u lambda=0 gamma=0.5 phi=0.6
```