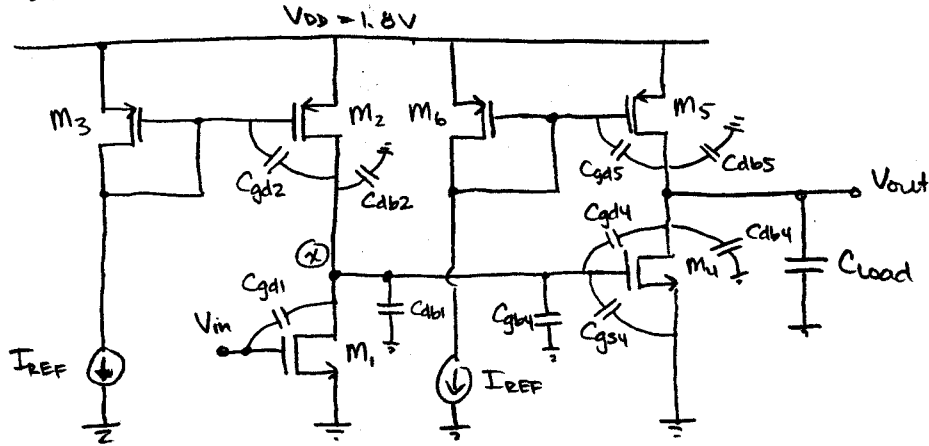


Homework 5, Fall 2004

- 1) All $W/L = 2/0.18$, $V_{DD} = 1.8V$, $I_{REF} = 10\mu A$. Assume wells of all devices are tied to their respective sources. DC voltage at V_{in} is set to bias V_{out} at $0.9V$.



- a) The two poles will be associated with node x and the output. There is no pole associated with the input because there is no source resistance.

The resistance at node x is: $R_x = r_{o1} \parallel r_{o2} = \frac{1}{\lambda_n I_{D1}} \parallel \frac{1}{\lambda_p I_{D2}}$

$R_x = 400 \text{ k}\Omega$

The resistance at node V_{out} is: $R_{out} = r_{o4} \parallel r_{o5} = 400 \text{ k}\Omega$

For all transistors:

$C_{gd} = C_{gdo} \cdot W = (5 \times 10^{-10}) (2 \times 10^{-6}) = 1 \text{ fF}$

$C_{gb} = C_{gbo} \cdot L = (4 \times 10^{-10}) (0.18 \times 10^{-6}) = 0.072 \text{ fF}$

$C_{gs} = C_{gso} \cdot W + \frac{2}{3} C_{ox} WL = 4.36 \text{ fF}$

We assume that the source and drain regions are minimum size and have a length of $4\lambda = 4(0.09\mu m) = 0.36\mu m$.

Thus, area of source/drain = $4\lambda \cdot W = 0.72 \mu m^2$
 perimeter of source/drain = $8\lambda + W = 2.72 \mu m$

The voltage at node x is: $V_x = V_T + V_{DSAT} = 0.5 + \sqrt{\frac{2(10)}{140(2/0.18)}} = 0.613V$

So, $C_{db1} = \frac{C_J \cdot A_D}{(1 + \frac{V_{DB}}{PB})^{m_{JS}}} + \frac{C_{JSW} \cdot P_S}{(1 + \frac{V_{DB}}{PB})^{m_{JSW}}}$
 $= \frac{(6 \times 10^{-4}) (0.72 \times (10^{-6})^2)}{(1 + \frac{0.613}{0.8})^{1/2}} + \frac{(2 \times 10^{-10}) (2.72 \times 10^{-6})}{(1 + \frac{0.613}{0.8})^{1/3}} = 0.775 \text{ fF}$

$C_{db2} = 0.676 \text{ fF}$

Homework 5, Fall 2004

1) a) (cont.)

The voltage at $V_{out} = 0.9V$.

Thus,

$$C_{db4} = C_{db5} = \boxed{0.719 \text{ fF}}$$

From the sizes of these capacitors, we see that the dominant pole is located at node x due to the Miller capacitance.

The equivalent capacitance at node x is:

$$C_x = C_{gd1} + C_{db1} + C_{gd2} + C_{db2} + C_{gs4} + C_{gb4} + (1 + g_m R_{out}) C_{gd4}$$

$$= 1 + 0.775 + 1 + 0.676 + 4.36 + 0.072 + (1 + (176\mu)(400k))(1) \text{ fF}$$

$$= \boxed{80 \text{ fF}}$$

$$\therefore \omega_{p1} = \frac{1}{R_x C_x} = \frac{1}{(400k)(80 \text{ fF})} = 31.25 \text{ Mrad/s} \Rightarrow \boxed{5 \text{ MHz}}$$

$$\omega_{p2} = \frac{1}{\frac{1}{g_m} (C_{gd1} + C_{db1} + C_{gd2} + C_{db2} + C_{gb4} + C_{gs4} + C_{db4} + C_{gd5} + C_{db5})}$$

$$= \frac{1}{\left(\frac{1}{176\mu S}\right) (1 + 0.775 + 1 + 0.676 + 0.072 + 4.36 + 0.719 + 1 + 0.719 \text{ fF})}$$

$$= 17 \text{ Grad/s} \Rightarrow \boxed{2.7 \text{ GHz}}$$

From hand calculations, the poles are at:

$$f_{p1} = 5 \text{ MHz}$$

$$f_{p2} = 2.7 \text{ GHz}$$

From SPICE: $f_{p1} = 4 \text{ MHz}$
 $f_{p2} = 675 \text{ MHz}$

The dominant pole is off due to the error in g_m, r_o caused by the large value for λ .

The nondominant pole is further off because the C_{gd4} is not actually that large, and C_{out} begins to reduce the output impedance causing the Miller cap to have less of an effect.

Homework 5, Fall 2004

1) c) When $C_{load} = 10 \text{ pF}$, the dominant pole is located at the output.

$$\omega_{p1} = \frac{1}{R_{out} C_{load}} = \frac{1}{(400 \text{ k} \times 10 \text{ pF})} = 250 \text{ krad/s} \Rightarrow \boxed{40 \text{ kHz}}$$

$$\begin{aligned} \omega_{p2} &= \frac{1}{R_x (C_{gd1} + C_{db1} + C_{gd2} + C_{db2} + C_{gs4} + C_{gs4} + C_{gd4})} \\ &= \frac{1}{(400 \text{ k})(1 + 0.775 + 1 + 0.676 + 0.072 + 4.36 + 1 \text{ fF})} \\ &= 281 \text{ Mrad/s} \Rightarrow \boxed{45 \text{ MHz}} \end{aligned}$$

From hand calculations: $f_{p1} = 40 \text{ kHz}$
 $f_{p2} = 45 \text{ MHz}$

From SPICE: $f_{p1} = 36 \text{ kHz}$
 $f_{p2} = 38 \text{ MHz}$

These values are sufficiently close.

Homework 5, Fall 2004

* hw8, 1: common-source, common-source amplifier

```
.model nch nmos level=1 tox=25 vto=0.5 kp=140e-6 lambda=0.1 gamma=0.5 phi=0.6
+capop=0 cgso=5e-10 cgdo=5e-10 cgbo=4e-10 cj=6e-4 cjsw=2e-10
```

```
.model pch pmos level=1 tox=25 vto=-0.5 kp=65e-6 lambda=0.15 gamma=0.5 phi=0.6
+capop=0 cgso=5e-10 cgdo=5e-10 cgbo=4e-10 cj=6e-4 cjsw=2e-10
```

```
.param w = 2u
.param l = 0.18u
.param lambda = 0.09u
.param a = '4*lambda*w'
.param p = '8*lambda+w'
```

```
vdd vdd 0 1.8
```

```
* set up ac input source
vin vin 0 0.614 ac 1
```

```
m1 1 vin 0 0 nch w=w l=l ad=a pd=p as=a ps=p
m2 1 2 vdd vdd pch w=w l=l ad=a pd=p as=a ps=p
m3 2 2 vdd vdd pch w=w l=l ad=a pd=p as=a ps=p
m4 out 1 0 0 nch w=w l=l ad=a pd=p as=a ps=p
m5 out 3 vdd vdd pch w=w l=l ad=a pd=p as=a ps=p
m6 3 3 vdd vdd pch w=w l=l ad=a pd=p as=a ps=p
i1 2 0 10u
i2 3 0 10u
```

```
cload out 0 0p
```

```
.options post=2 nomod captab pztol=1e-4 unwrap
```

```
.meas dc vbias find v(vin) when v(out)=0.9
```

```
.probe ac vdb(out) vp(out)
```

```
.op
```

```
.dc vin 0.613 0.617 0.01m
```

```
.pz v(out) vin
```

```
.ac dec 10 1k 1g
```

```
.alter
```

```
***** operating point information tnom= 25.000 temp= 25.000
```

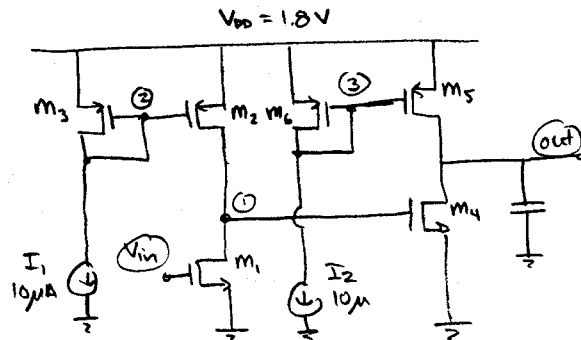
```
*****
```

```
***** operating point status is all simulation time is 0.
```

node	=voltage	node	=voltage	node	=voltage
+0:1	= 610.2628m	0:2	= 1.1412	0:3	= 1.1412
+0:out	= <u>909.5851m</u>	0:vdd	= 1.8000	0:vin	= 614.0000m

```
**** mosfets
```

```
subckt
element 0:m1 0:m2 0:m3 0:m4 0:m5 0:m6
model 0:nch 0:pch 0:pch 0:nch 0:pch 0:pch
id 10.7249u -10.7249u -10.0000u 10.3162u -10.3162u -10.0000u
```



Homework 5, Fall 2004

ibs	0.	0.	0.	0.	0.	0.
ibd	-6.1026f	11.8974f	6.5875f	-9.0959f	8.9041f	6.5875f
vgs	614.0000m	-658.7515m	-658.7515m	610.2628m	-658.7515m	-658.7515m
vds	610.2628m	-1.1897	-658.7515m	909.5851m	-890.4149m	-658.7515m
vbs	0.	0.	0.	0.	0.	0.
vth	500.0000m	-500.0000m	-500.0000m	500.0000m	-500.0000m	-500.0000m
vdsat	114.0000m	-158.7515m	-158.7515m	110.2628m	-158.7515m	-158.7515m
beta	1.6505m	851.1104u	793.5870u	1.6970m	818.6838u	793.5870u
gam eff	500.0000m	500.0000m	500.0000m	500.0000m	500.0000m	500.0000m
gm	188.1553u	135.1150u	125.9831u	187.1211u	129.9672u	125.9831u
gds	1.0108u	1.3651u	1.3651u	945.6129n	1.3651u	1.3651u
gmb	60.7269u	43.6082u	40.6609u	60.3931u	41.9467u	40.6609u
cdtot	1.7766f	1.6767f	1.7661f	1.7189f	1.7222f	1.7661f
cgtot	5.3870f	5.3870f	5.3870f	5.3870f	5.3870f	5.3870f
cstot	5.2910f	5.2910f	5.2910f	5.2910f	5.2910f	5.2910f
cbtot	1.8246f	1.7247f	1.8141f	1.7669f	1.7702f	1.8141f
cgs	4.3150f	4.3150f	4.3150f	4.3150f	4.3150f	4.3150f
cgd	1.0000f	1.0000f	1.0000f	1.0000f	1.0000f	1.0000f

***** pole/zero analysis tnom= 25.000 temp= 25.000

input = 0:vin output = v(out)

poles (rad/sec) poles (hertz)

real	imag	real	imag
-25.0082x	0.	-3.9802x	0.
-4.2458g	0.	-675.7327x	0.
-13.3910g	0.	-2.1312g	0.
-19.9427g	0.	-3.1740g	0.

poles for
C_{load} = 0 pF

zeros (rad/sec) zeros (hertz)

real	imag	real	imag
-12.0822g	0.	-1.9229g	0.
-12.0822g	0.	-1.9229g	0.

oload out 0 10p * change the load to 10 pf

.end

**** operating point status is all simulation time is 0.

node	=voltage	node	=voltage	node	=voltage
------	----------	------	----------	------	----------

+0:1	= 610.2628m	0:2	= 1.1412	0:3	= 1.1412
+0:out	= 909.5851m	0:vdd	= 1.8000	0:vin	= 614.0000m

**** mosfets

subckt	element	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6
	model	0:nch	0:pch	0:pch	0:nch	0:pch	0:pch
	id	10.7249u	-10.7249u	-10.0000u	10.3162u	-10.3162u	-10.0000u

Homework 5, Fall 2004

ibs	0.	0.	0.	0.	0.	0.
ibd	-6.1026f	11.8974f	6.5875f	-9.0959f	8.9041f	6.5875f
vgs	614.0000m	-658.7515m	-658.7515m	610.2628m	-658.7515m	-658.7515m
vds	610.2628m	-1.1897	-658.7515m	909.5851m	-890.4149m	-658.7515m
vbs	0.	0.	0.	0.	0.	0.
vth	500.0000m	-500.0000m	-500.0000m	500.0000m	-500.0000m	-500.0000m
vdsat	114.0000m	-158.7515m	-158.7515m	110.2628m	-158.7515m	-158.7515m
beta	1.6505m	851.1104u	793.5870u	1.6970m	818.6838u	793.5870u
gam eff	500.0000m	500.0000m	500.0000m	500.0000m	500.0000m	500.0000m
gm	188.1553u	135.1150u	125.9831u	187.1211u	129.9672u	125.9831u
gds	1.0108u	1.3651u	1.3651u	945.6129n	1.3651u	1.3651u
gmb	60.7269u	43.6082u	40.6609u	60.3931u	41.9467u	40.6609u
cdtot	1.7766f	1.6767f	1.7661f	1.7189f	1.7222f	1.7661f
cgtot	5.3870f	5.3870f	5.3870f	5.3870f	5.3870f	5.3870f
cstot	5.2910f	5.2910f	5.2910f	5.2910f	5.2910f	5.2910f
cbtot	1.8246f	1.7247f	1.8141f	1.7669f	1.7702f	1.8141f
cgs	4.3150f	4.3150f	4.3150f	4.3150f	4.3150f	4.3150f
cgd	1.0000f	1.0000f	1.0000f	1.0000f	1.0000f	1.0000f

***** pole/zero analysis tnom= 25.000 temp= 25.000

input = 0:vin output = v(out)

poles (rad/sec) poles (hertz)

real	imag	real	imag
-229.1634k	0.	-36.4725k	0.
-241.2804x	0.	-38.4010x	0.
-12.0835g	0.	-1.9232g	0.
-13.7116g	0.	-2.1823g	0.

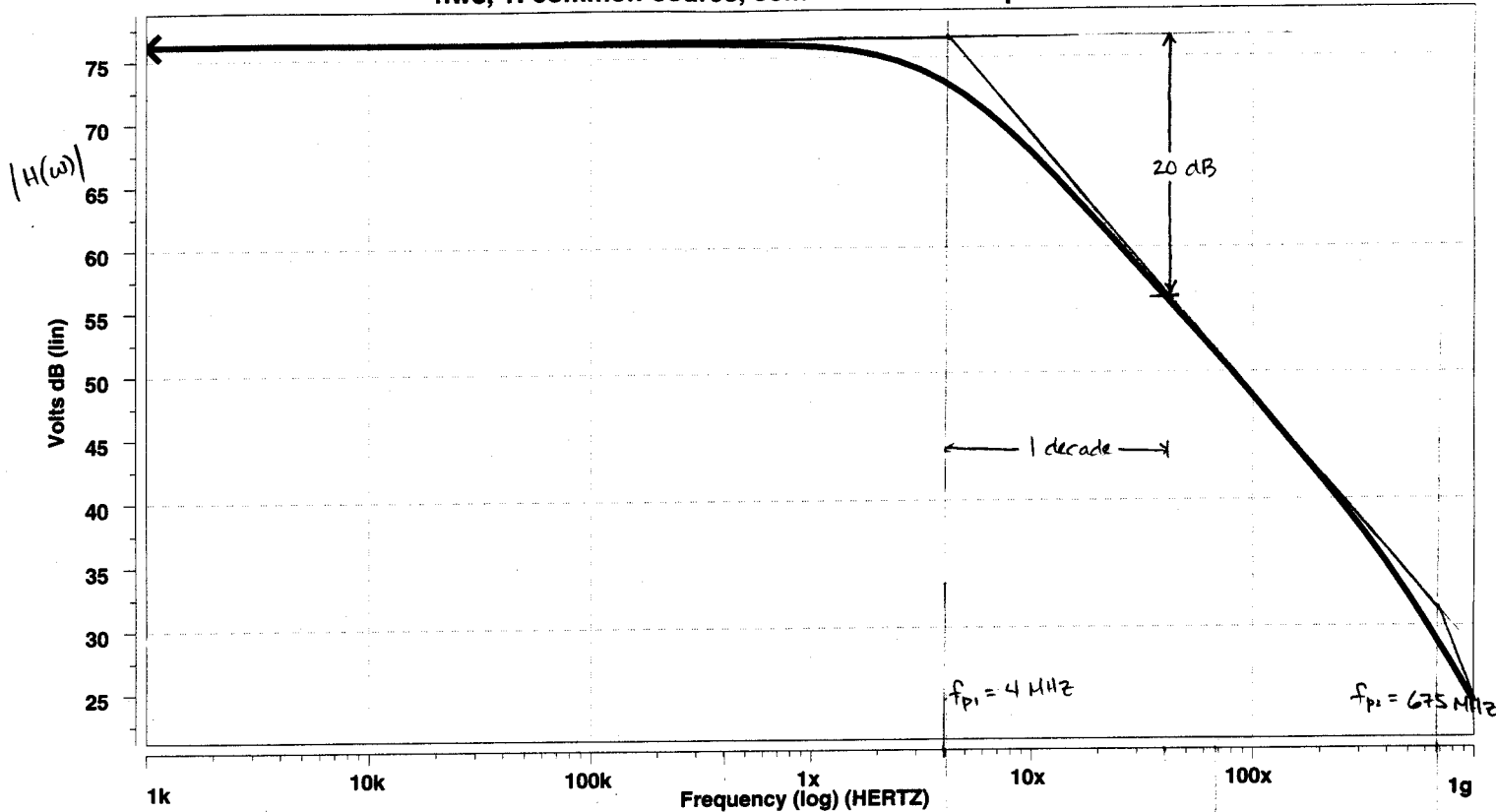
poles for
C_{load} = 10 pF

zeros (rad/sec) zeros (hertz)

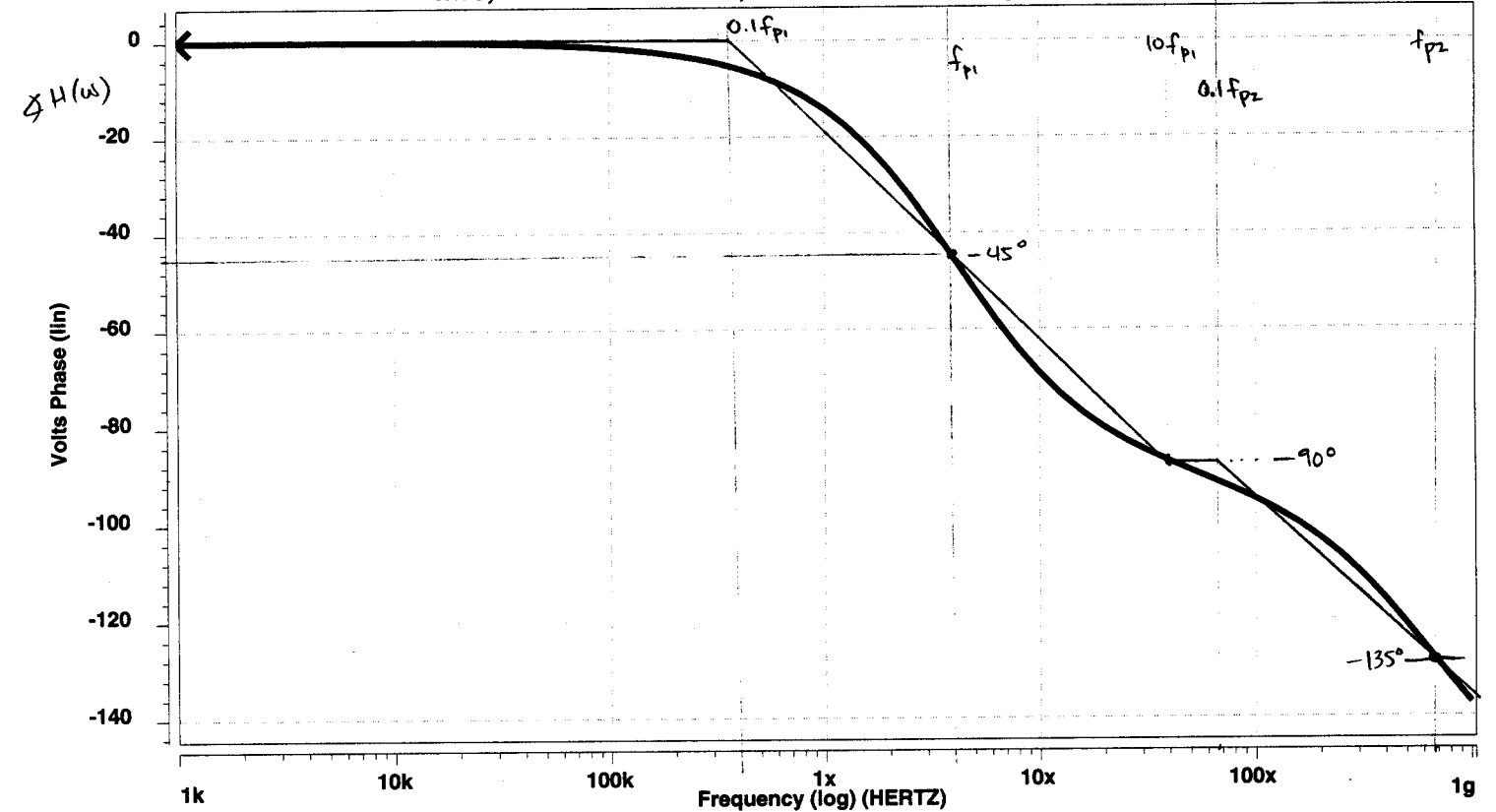
real	imag	real	imag
-12.0822g	0.	-1.9229g	0.
-12.0822g	0.	-1.9229g	0.

$C_{LOAD} = 0PF$

* hw8, 1: common-source, common-source amplifier

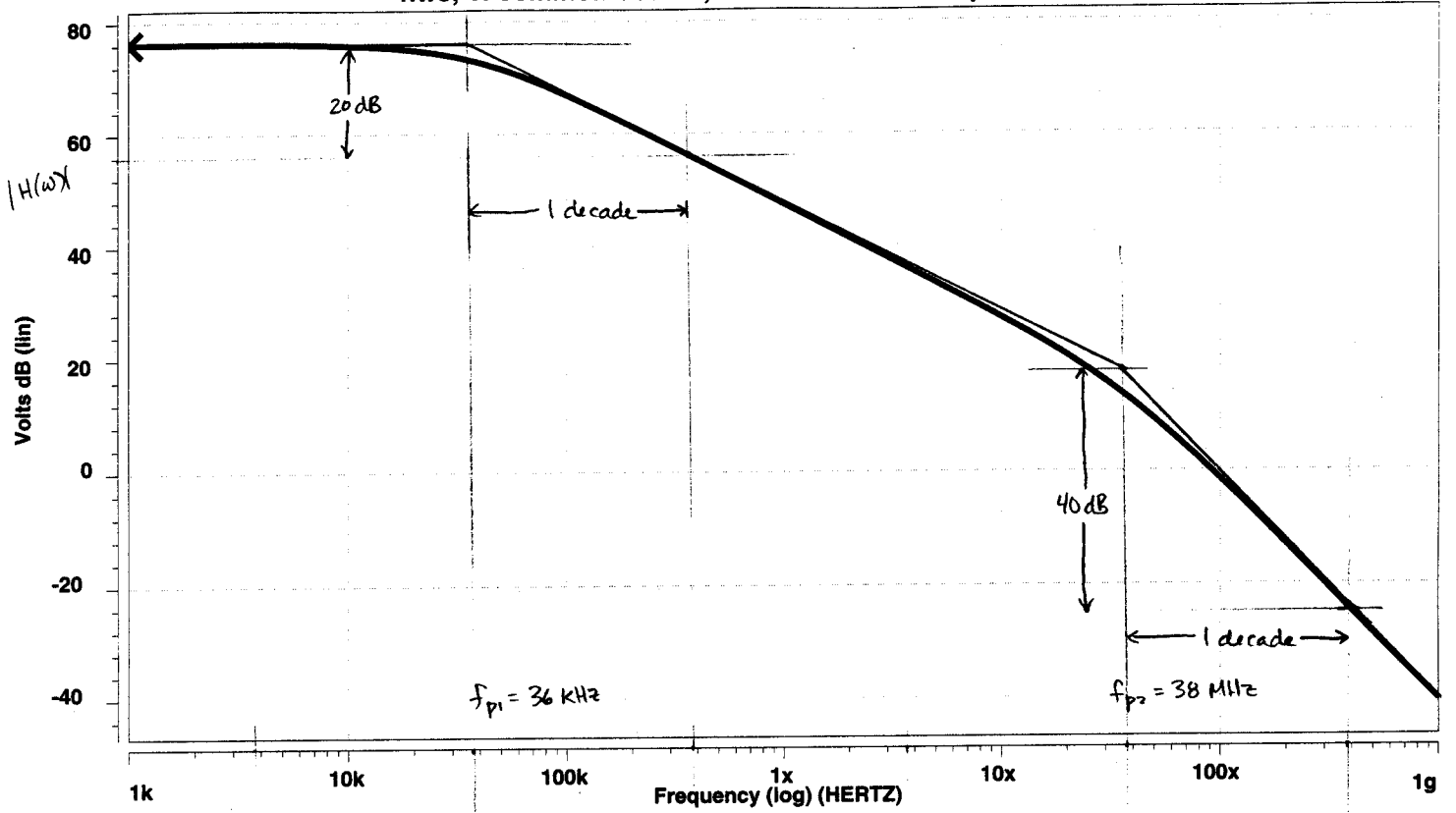


* hw8, 1: common-source, common-source amplifier

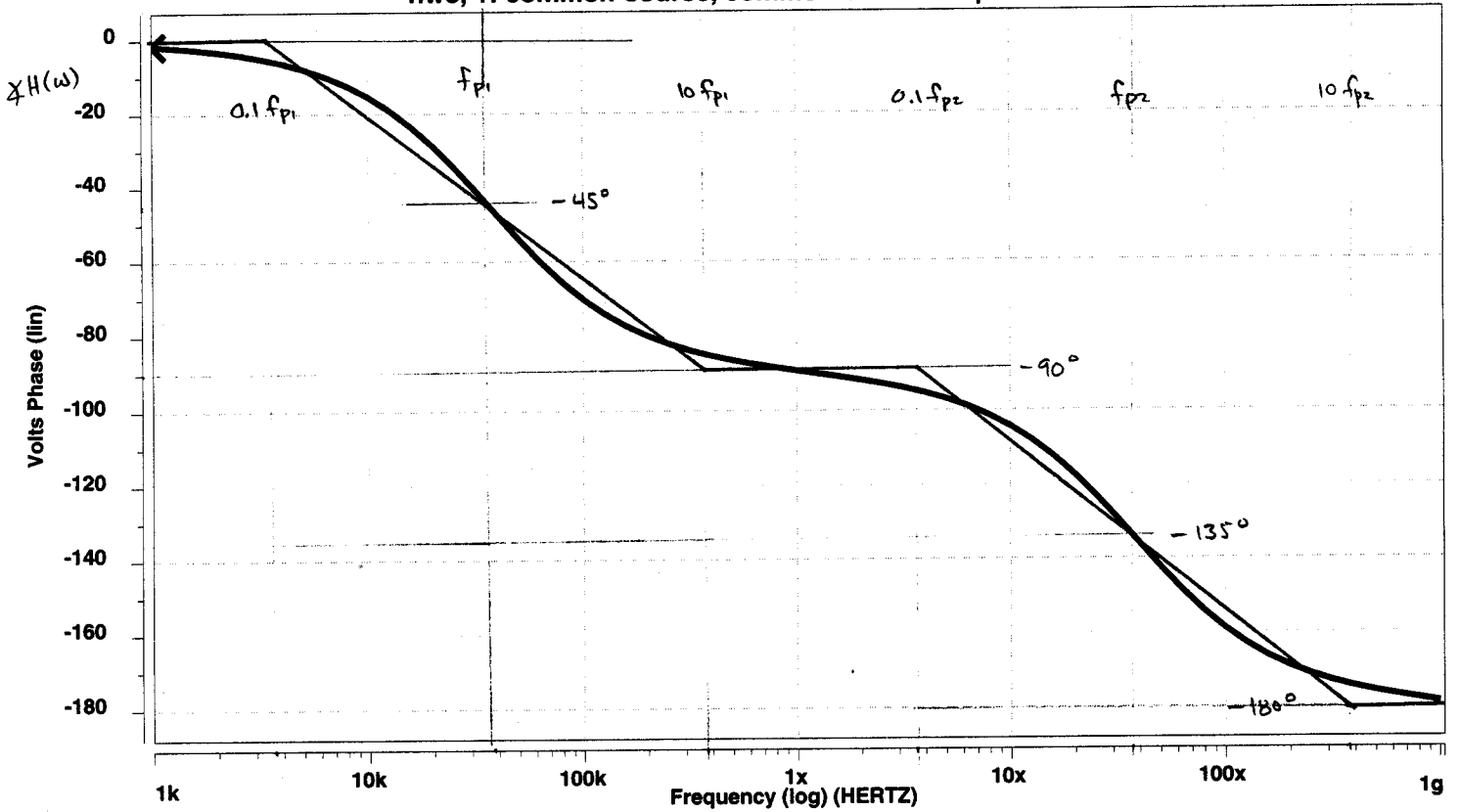


$C_{LOAD} = 10 \text{ pF}$

* hw8, 1: common-source, common-source amplifier

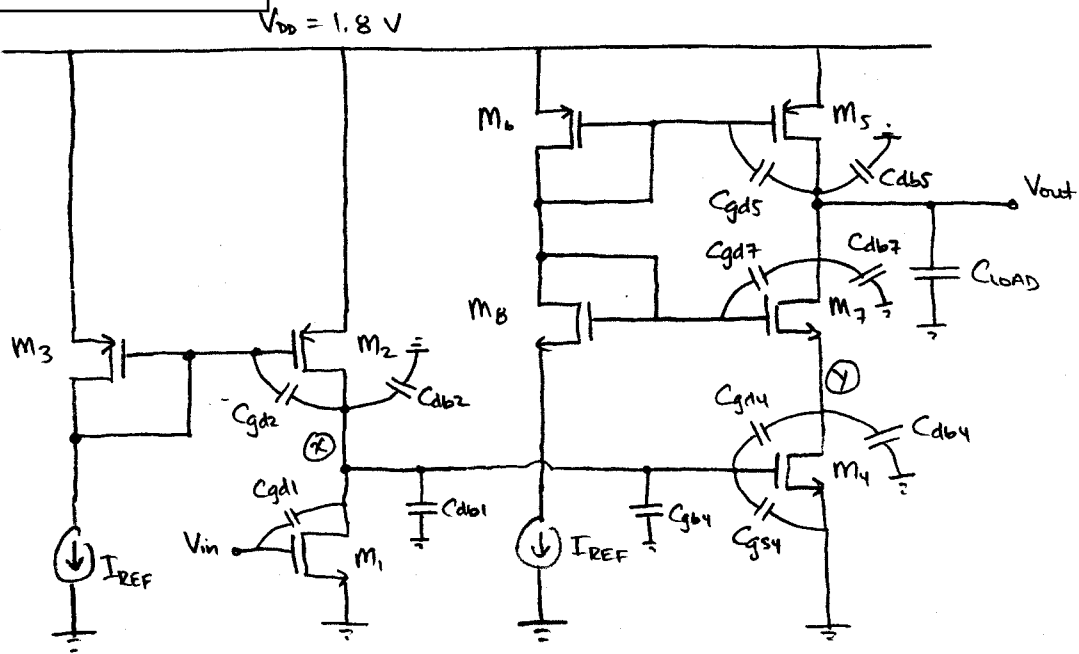


* hw8, 1: common-source, common-source amplifier



Homework 5, Fall 2004

2)



a) The two poles will be associated with node x and the output. Due to the common-gate configuration of M7, the impedance at node y is very small, so this is not one of the first two poles.

$$R_x = 400 \text{ k}\Omega, \quad R_{out} \approx r_{os} = 666 \text{ k}\Omega$$

This is very similar to the previous problem, except the large Miller capacitance is no longer present due to the common-gate stage.

$$\omega_{p1} = \frac{1}{R_x (C_{gd1} + C_{db1} + C_{gd2} + C_{db2} + C_{gb4} + C_{gs4} + (1 + g_m \left(\frac{r_{os} + r_{o7}}{1 + g_m r_{o7}} \right)) C_{gd4}}$$

$$= \frac{1}{(400 \text{ k}\Omega \times (1 + 0.775 + 1 + 0.676 + 0.072 + 4.36 + (1 + 1 + \frac{0.1}{0.15})) (1) \text{ f})}$$

$$= 236 \text{ Mrad/s} \Rightarrow \boxed{37.7 \text{ MHz}}$$

$$\omega_{p2} = \frac{1}{R_{out} (C_{gd5} + C_{db5} + C_{gd7} + C_{db7})}$$

$$= \frac{1}{(666 \text{ k}\Omega \times (1 + 0.719 + 1 + 0.719))} = 436 \text{ Mrad/s} \Rightarrow \boxed{69 \text{ MHz}}$$

Homework 5, Fall 2004

2) a) (cont.)

From hand calculations, $f_{p1} = 37.7 \text{ MHz}$
 $f_{p2} = 69 \text{ MHz}$.

From SPICE: $f_{p1} = 32 \text{ MHz}$
 $f_{p2} = 44 \text{ MHz}$

These values are relatively close. The main discrepancy is due to the incorrect values for r_o , and assuming that the capacitors going to nodes with impedance $\frac{1}{g_m}$ actually go to ground.

c) When $C_{load} = 10 \text{ pF}$, the dominant pole is at the output, and the pole associated with node x does not change much.

$$\omega_{p1} = \frac{1}{R_{out} C_{load}} = \frac{1}{(666 \text{ k}\Omega)(10 \text{ pF})} = 150 \text{ Mrad/s} \Rightarrow \boxed{24 \text{ kHz}}$$

$$\omega_{p2} = \frac{1}{R_x (C_{gd1} + C_{db1} + C_{gd2} + C_{db2} + C_{gb4} + C_{gs4} + 2C_{gd4})}$$

$$= 230 \text{ Mrad/s} \Rightarrow \boxed{36.5 \text{ MHz}}$$

From hand calculations: $f_{p1} = 24 \text{ kHz}$
 $f_{p2} = 36.5 \text{ MHz}$

From SPICE: $f_{p1} = 22 \text{ MHz}$
 $f_{p2} = 35 \text{ MHz}$

These values are pretty close

Homework 5, Fall 2004

* hw8, 2: common-source, common-source amplifier with cascode

```
.model nch nmos level=1 tox=25 vto=0.5 kp=140e-6 lambda=0.1 gamma=0.5 phi=0.6
+capop=0 cgso=5e-10 cgdo=5e-10 cgbo=4e-10 cj=6e-4 cjsw=2e-10
```

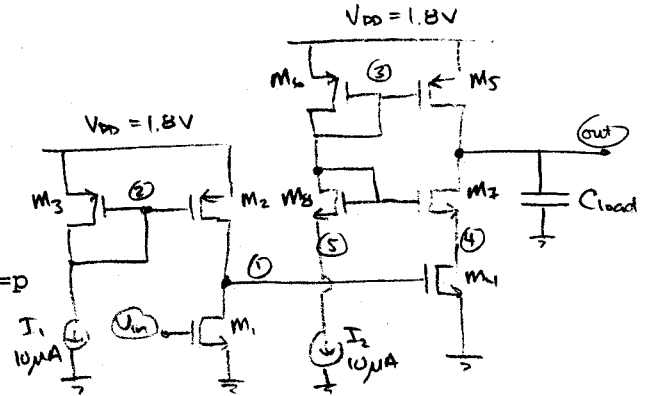
```
.model pch pmos level=1 tox=25 vto=-0.5 kp=65e-6 lambda=0.15 gamma=0.5 phi=0.6
+capop=0 cgso=5e-10 cgdo=5e-10 cgbo=4e-10 cj=6e-4 cjsw=2e-10
```

```
.param w = 2u
.param l = 0.18u
.param lambda = 0.09u
.param a = '4*lambda*w'
.param p = '8*lambda+w'
```

```
vdd vdd 0 1.8
```

```
* set up ac input source
vin vin 0 0.61397 ac 1
```

```
m1 1 vin 0 0 nch w=w l=l ad=a pd=p as=a ps=p
m2 1 2 vdd vdd pch w=w l=l ad=a pd=p as=a ps=p
m3 2 2 vdd vdd pch w=w l=l ad=a pd=p as=a ps=p
m4 3 1 0 0 nch w=w l=l ad=a pd=p as=a ps=p
m5 out 4 vdd vdd pch w=w l=l ad=a pd=p as=a ps=p
m6 4 4 vdd vdd pch w=w l=l ad=a pd=p as=a ps=p
m7 out 4 3 3 nch w=w l=l ad=a pd=p as=a ps=p
m8 4 4 5 5 nch w=w l=l ad=a pd=p as=a ps=p
i1 2 0 10u
i2 5 0 10u
```



```
clload out 0 0p
```

```
.options post=2 nomod captab pztol=1e-4 unwrap
```

```
.meas dc vbias find v(vin) when v(out)=0.9
```

```
.probe ac vdb(out) vp(out)
```

```
.op
```

```
.dc vin 0.613 0.617 0.01m
```

```
.pz v(out) vin
```

```
.ac dec 10 1k 1g
```

```
.alter
```

```
***** operating point information tnom= 25.000 temp= 25.000
```

```
*****
```

```
***** operating point status is all simulation time is 0.
```

node	=voltage	node	=voltage	node	=voltage
+0:1	= 612.6388m	0:2	= 1.1412	0:3	= 527.5326m
+0:4	= 1.1412	0:5	= 531.1674m	0:out	= 856.5649m
+0:vdd	= 1.8000	0:vin	= 613.9700m		

```
**** mosfets
```

Homework 5, Fall 2004

subckt element	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6
model	0:nch	0:pch	0:pch	0:nch	0:pch	0:pch
id	10.7216u	-10.7216u	-10.0000u	10.3886u	-10.3886u	-10.0000u
ibs	0.	0.	0.	0.	0.	0.
ibd	-6.1264f	11.8736f	6.5875f	-5.2753f	9.4344f	6.5875f
vgs	613.9700m	-658.7515m	-658.7515m	612.6388m	-658.7515m	-658.7515m
vds	612.6388m	-1.1874	-658.7515m	527.5326m	-943.4351m	-658.7515m
vbs	0.	0.	0.	0.	0.	0.
vth	500.0000m	-500.0000m	-500.0000m	500.0000m	-500.0000m	-500.0000m
vdsat	113.9700m	-158.7515m	-158.7515m	112.6388m	-158.7515m	-158.7515m
beta	1.6509m	850.8530u	793.5870u	1.6376m	824.4277u	793.5870u
gam eff	500.0000m	500.0000m	500.0000m	500.0000m	500.0000m	500.0000m
gm	188.1479u	135.0742u	125.9831u	184.4591u	130.8791u	125.9831u
gds	1.0103u	1.3651u	1.3651u	986.8052n	1.3651u	1.3651u
gmb	60.7245u	43.5950u	40.6609u	59.5339u	42.2410u	40.6609u
cdtot	1.7760f	1.6770f	1.7661f	1.7956f	1.7133f	1.7661f
cgtot	5.3870f	5.3870f	5.3870f	5.3870f	5.3870f	5.3870f
cstot	5.2910f	5.2910f	5.2910f	5.2910f	5.2910f	5.2910f
cbtot	1.8240f	1.7250f	1.8141f	1.8436f	1.7613f	1.8141f
cgs	4.3150f	4.3150f	4.3150f	4.3150f	4.3150f	4.3150f
cgd	1.0000f	1.0000f	1.0000f	1.0000f	1.0000f	1.0000f

subckt element	0:m7	0:m8
model	0:nch	0:nch
id	10.3886u	10.0000u
ibs	0.	0.
ibd	-3.2903f	-6.1008f
vgs	613.7160m	610.0811m
vds	329.0323m	610.0811m
vbs	0.	0.
vth	500.0000m	500.0000m
vdsat	113.7160m	110.0811m
beta	1.6067m	1.6505m
gam eff	500.0000m	500.0000m
gm	182.7118u	181.6842u
gds	1.0058u	942.4997n
gmb	58.9700u	58.6383u
cdtot	1.8492f	1.7766f
cgtot	5.3870f	5.3870f
cstot	5.2910f	5.2910f
cbtot	1.8972f	1.8246f
cgs	4.3150f	4.3150f
cgd	1.0000f	1.0000f

***** pole/zero analysis tnom= 25.000 temp= 25.000

input = 0:vin output = v(out)

poles (rad/sec) poles (hertz)

real	imag	real	imag
-205.7070x	0.	-32.7393x	0.
-276.3565x	0.	-43.9835x	0.
-13.0711g	0.	-2.0803g	0.
-20.8381g	0.	-3.3165g	0.
-25.3158g	0.	-4.0291g	0.

zeros (rad/sec) zeros (hertz)

poles for
 $C_{load} = 0 pF$

Homework 5, Fall 2004

real	imag	real	imag
-12.0822g	0.	-1.9229g	0.
-18.9192g	0.	-3.0111g	0.

cloud out 0 10p * change the load to 10 pf

.end

***** operating point information tnom= 25.000 temp= 25.000

**** operating point status is all simulation time is 0.

node	=voltage	node	=voltage	node	=voltage
+0:1	= 612.6388m	0:2	= 1.1412	0:3	= 527.5326m
+0:4	= 1.1412	0:5	= 531.1674m	0:out	= 856.5649m
+0:vdd	= 1.8000	0:vin	= 613.9700m		

**** mosfets

subckt	element	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6
	model	0:nch	0:pch	0:pch	0:nch	0:pch	0:pch
	id	10.7216u	-10.7216u	-10.0000u	10.3886u	-10.3886u	-10.0000u
	ibs	0.	0.	0.	0.	0.	0.
	ibd	-6.1264f	11.8736f	6.5875f	-5.2753f	9.4344f	6.5875f
	vgs	613.9700m	-658.7515m	-658.7515m	612.6388m	-658.7515m	-658.7515m
	vds	612.6388m	-1.1874	-658.7515m	527.5326m	-943.4351m	-658.7515m
	vbs	0.	0.	0.	0.	0.	0.
	vth	500.0000m	-500.0000m	-500.0000m	500.0000m	-500.0000m	-500.0000m
	vdsat	113.9700m	-158.7515m	-158.7515m	112.6388m	-158.7515m	-158.7515m
	beta	1.6509m	850.8530u	793.5870u	1.6376m	824.4277u	793.5870u
	gam eff	500.0000m	500.0000m	500.0000m	500.0000m	500.0000m	500.0000m
	gm	188.1479u	135.0742u	125.9831u	184.4591u	130.8791u	125.9831u
	gds	1.0103u	1.3651u	1.3651u	986.8052n	1.3651u	1.3651u
	gmb	60.7245u	43.5950u	40.6609u	59.5339u	42.2410u	40.6609u
	cdtot	1.7760f	1.6770f	1.7661f	1.7956f	1.7133f	1.7661f
	cgtot	5.3870f	5.3870f	5.3870f	5.3870f	5.3870f	5.3870f
	cstot	5.2910f	5.2910f	5.2910f	5.2910f	5.2910f	5.2910f
	cbtot	1.8240f	1.7250f	1.8141f	1.8436f	1.7613f	1.8141f
	cgs	4.3150f	4.3150f	4.3150f	4.3150f	4.3150f	4.3150f
	cgd	1.0000f	1.0000f	1.0000f	1.0000f	1.0000f	1.0000f

subckt	element	0:m7	0:m8
	model	0:nch	0:nch
	id	10.3886u	10.0000u
	ibs	0.	0.
	ibd	-3.2903f	-6.1008f
	vgs	613.7160m	610.0811m
	vds	329.0323m	610.0811m
	vbs	0.	0.
	vth	500.0000m	500.0000m
	vdsat	113.7160m	110.0811m
	beta	1.6067m	1.6505m
	gam eff	500.0000m	500.0000m

Homework 5, Fall 2004

gm	182.7118u	181.6842u
gds	1.0058u	942.4997n
gmb	58.9700u	58.6383u
cdtot	1.8492f	1.7766f
cgtot	5.3870f	5.3870f
cstot	5.2910f	5.2910f
cbtot	1.8972f	1.8246f
cgs	4.3150f	4.3150f
cgd	1.0000f	1.0000f

***** pole/zero analysis tnom= 25.000 temp= 25.000

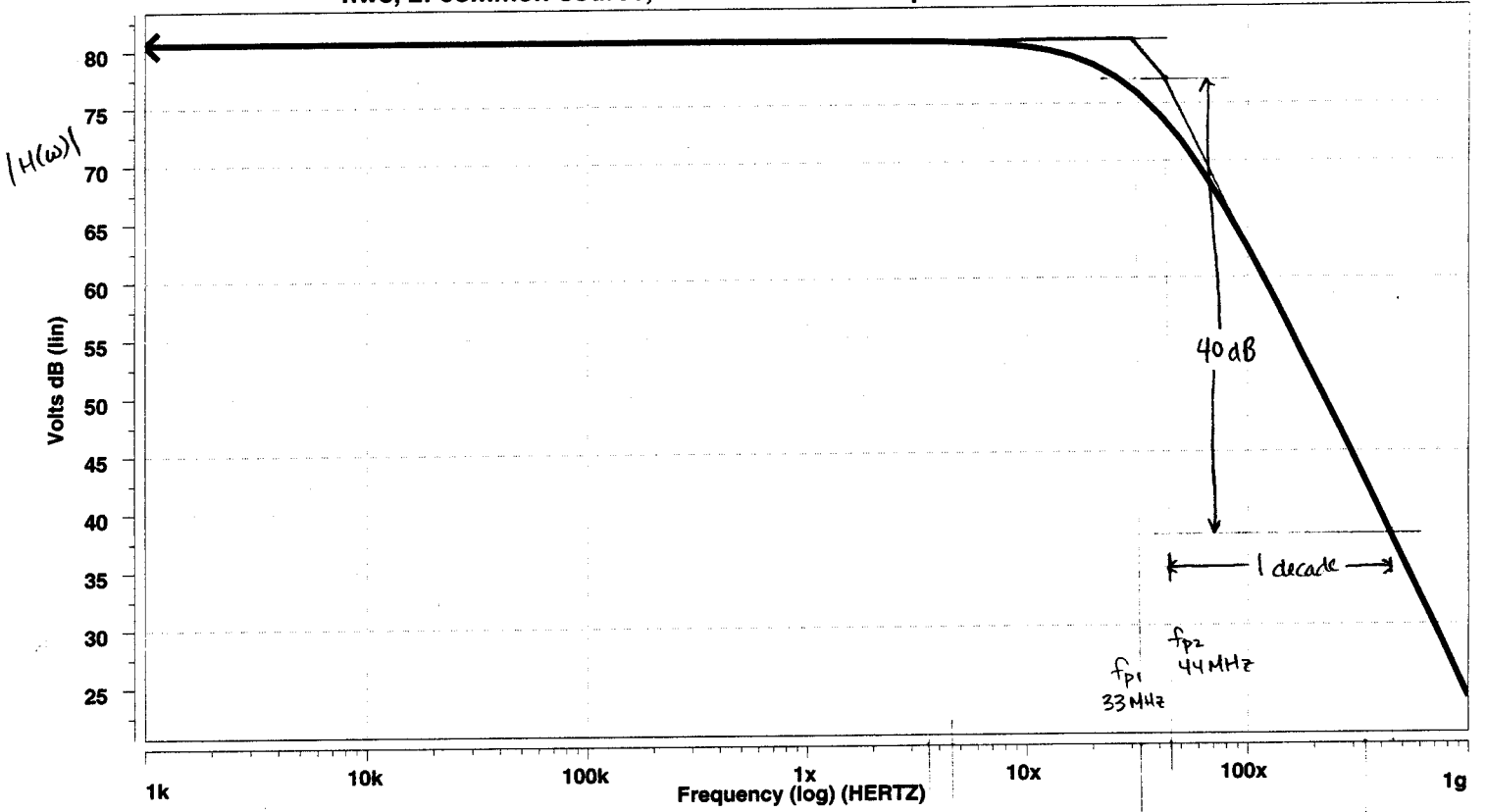
input = 0:vin output = v(out)

poles (rad/sec)		poles (hertz)	
real	imag	real	imag
-136.9762k	0.	-21.8004k	0.
-217.4785x	0.	-34.6128x	0.
-12.1375g	-690.5360x	-1.9317g	-109.9022x
-12.1375g	690.5360x	-1.9317g	109.9022x
-26.4176g	0.	-4.2045g	0.
zeros (rad/sec)		zeros (hertz)	
real	imag	real	imag
-12.0822g	0.	-1.9229g	0.
-18.9192g	0.	-3.0111g	0.

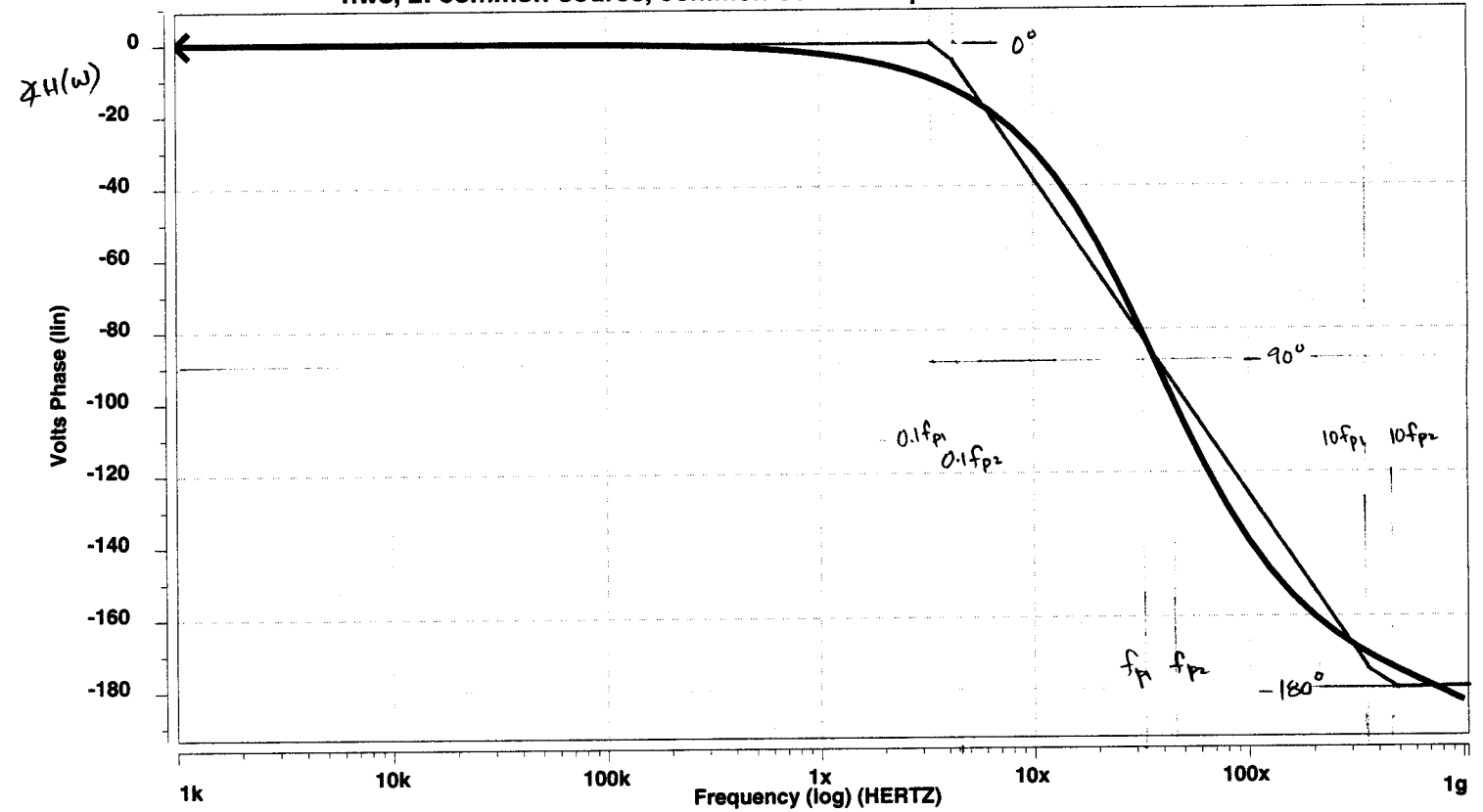
poles for
 Cload = 10pF

$C_{load} = 0pF$

* hw8, 2: common-source, common-source amplifier with cascode

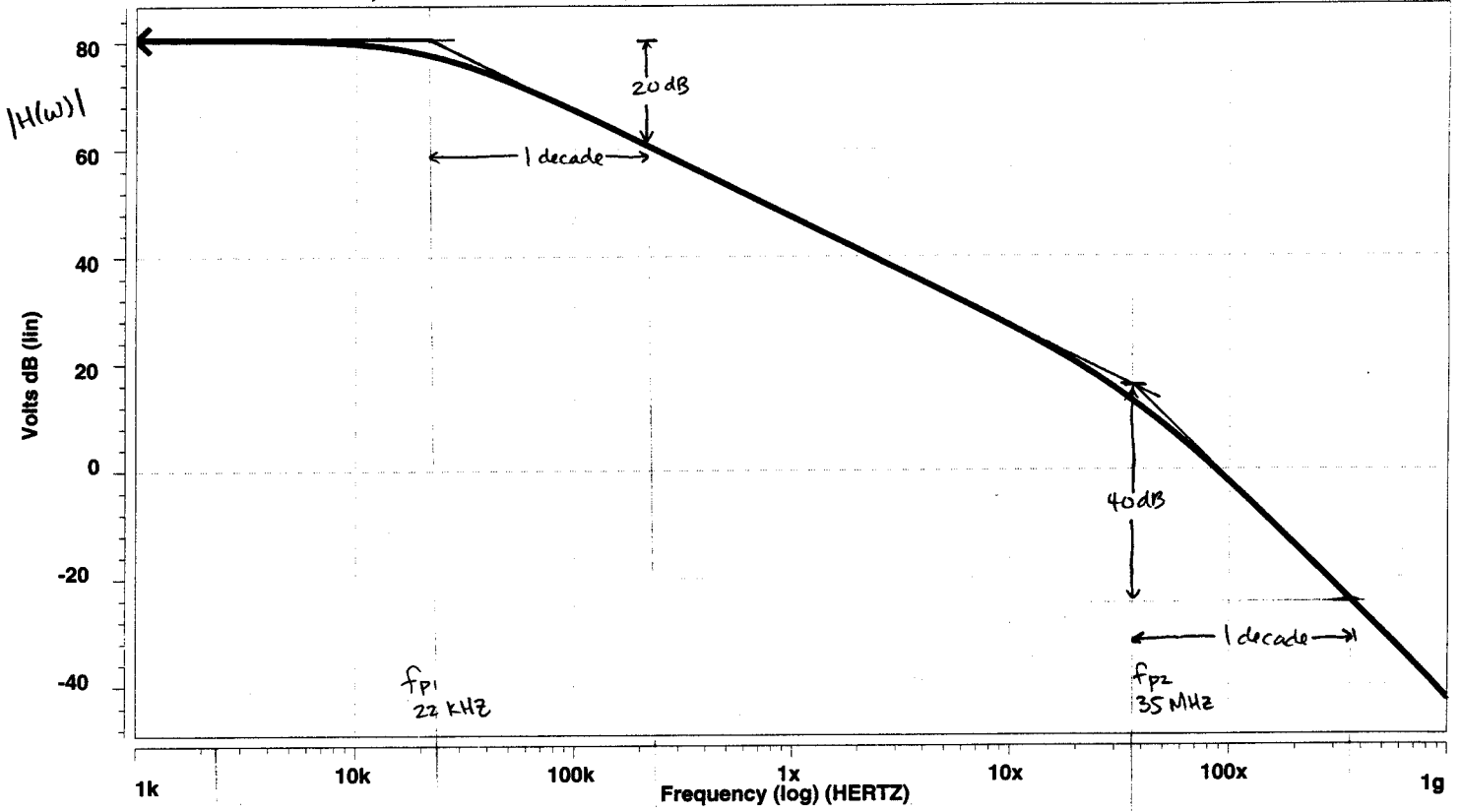


* hw8, 2: common-source, common-source amplifier with cascode

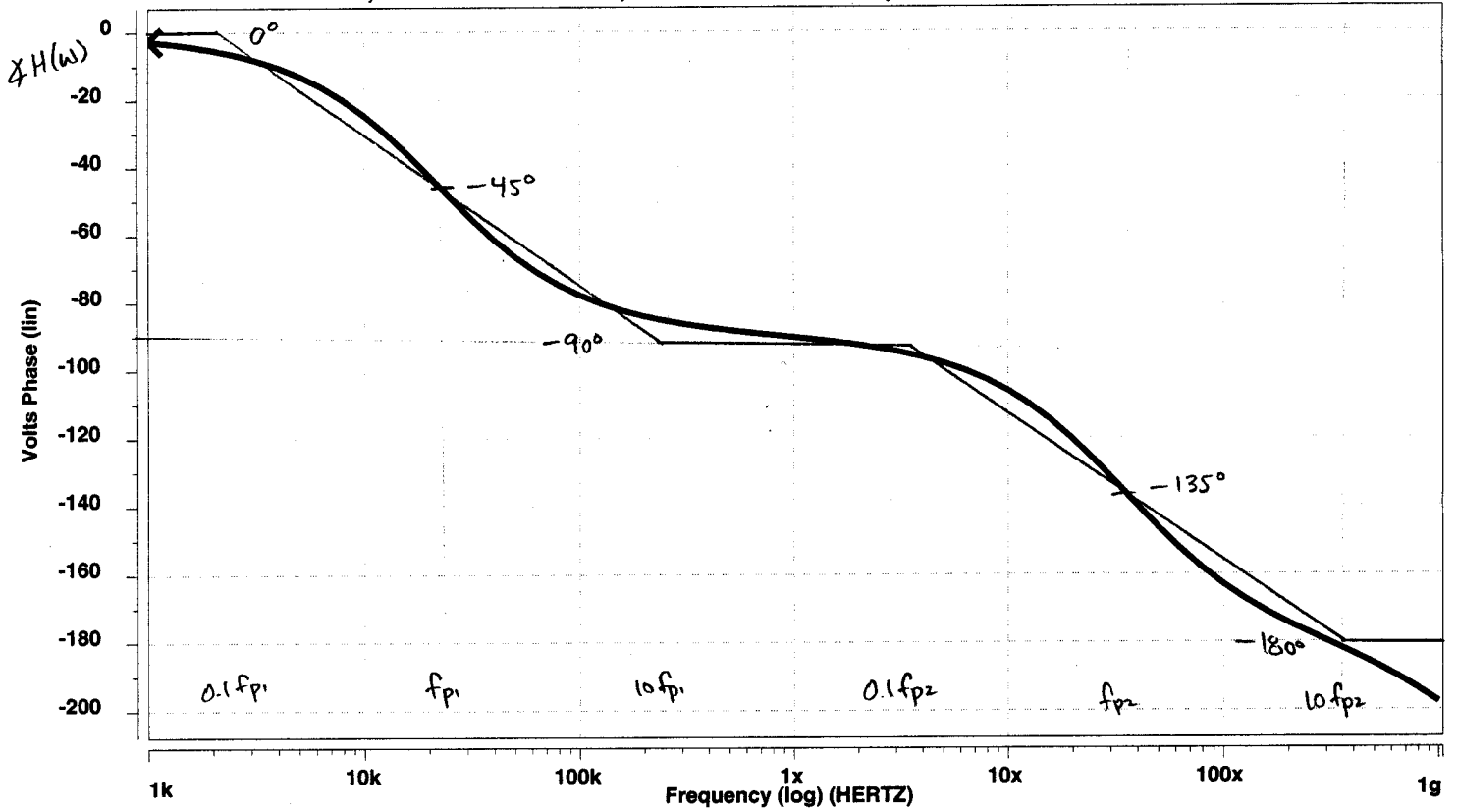


$C_{LOAD} = 10\text{ pF}$

* hw8, 2: common-source, common-source amplifier with cascode

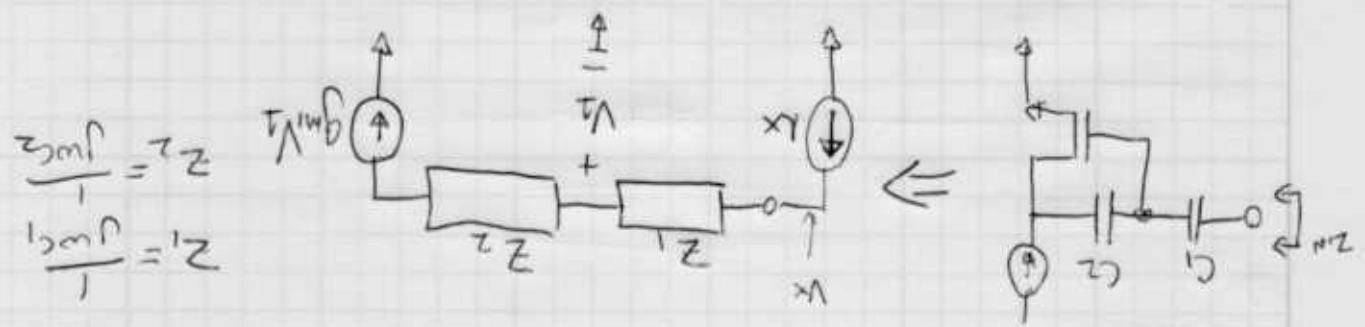


* hw8, 2: common-source, common-source amplifier with cascode

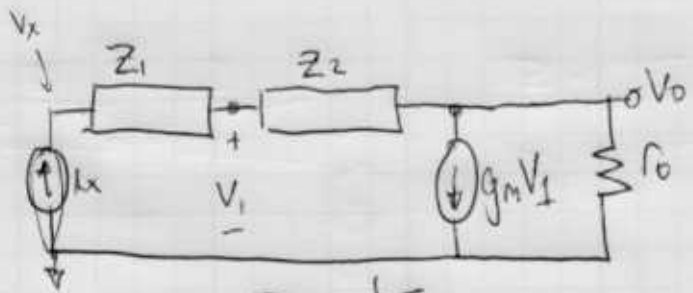
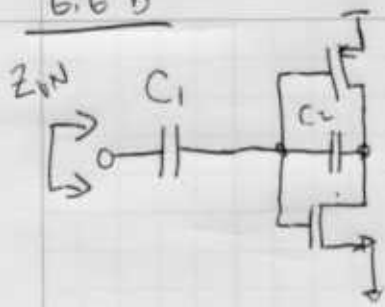


$$Z_{in} = \frac{V_x}{I_x} = \frac{1}{g_m} + Z_1 = \frac{1}{g_m(j\omega C_1)} = \frac{1}{j\omega C_1 + g_m}$$

- (1) $I_x = g_m V_1 \Rightarrow V_1 = \frac{I_x}{g_m}$
- (2) $V_x = V_1 + I_x \cdot Z_1$
- $\Rightarrow V_x = \frac{I_x}{g_m} + I_x \cdot Z_1$



6.6 b



$$Z_1 = \frac{1}{j\omega C_1}$$

$$Z_2 = \frac{1}{j\omega C_2}$$

$$g_m = g_{m1} + g_{m2}$$

$$r_o = r_{o1} \parallel r_{o2}$$

$$i_x = g_m V_1 + \frac{V_o}{r_o} \quad (1)$$

$$V_x = V_1 + i_x \cdot Z_1 \quad (2)$$

$$V_x = V_o + i_x \cdot Z_2 \quad (3)$$

~~1+2~~

$$(1+2) \Rightarrow i_x = g_m (V_x - i_x Z_1) + \frac{V_o}{r_o}$$

$$\Rightarrow i_x = g_m V_x - g_m Z_1 i_x + \frac{V_o}{r_o} \quad (4)$$

$$(2+3) \Rightarrow V_o = V_x - i_x (Z_1 + Z_2) \quad (5)$$

$$(4+5) \Rightarrow i_x = g_m V_x - g_m Z_1 i_x + \frac{V_x}{r_o} - i_x \frac{Z_1 + Z_2}{r_o}$$

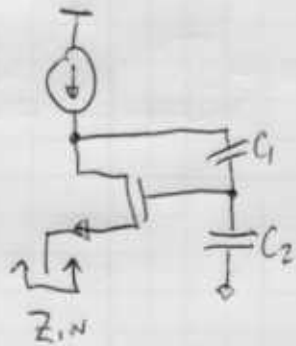
$$\Rightarrow i_x \left(1 + g_m Z_1 + \frac{Z_1 + Z_2}{r_o} \right) = V_x \left(g_m + \frac{1}{r_o} \right) \quad (6)$$

$$Z_{IN} \triangleq \frac{V_x}{i_x} = \frac{1 + g_m Z_1 + \frac{Z_1 + Z_2}{r_o}}{g_m + \frac{1}{r_o}} =$$

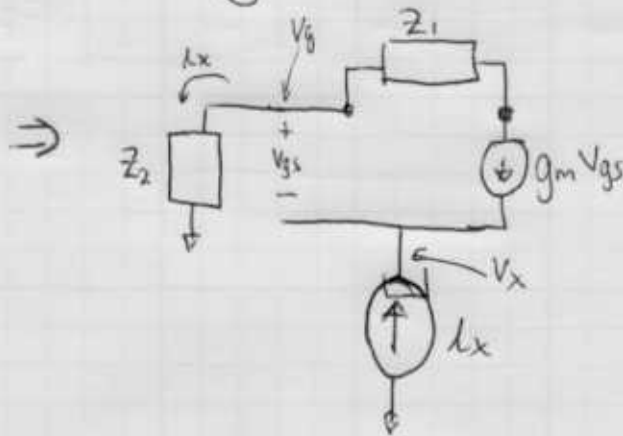
$$Z_{IN} = \frac{1 + \frac{g_{m1} + g_{m2}}{j\omega C_1} + \frac{1}{(r_{o1} \parallel r_{o2}) j\omega C_1} + \frac{1}{(r_{o1} \parallel r_{o2}) j\omega C_2}}{(g_{m1} + g_{m2}) + \frac{1}{r_{o1} \parallel r_{o2}}}$$

6.6c

Homework 5, Fall 2004



Assume $\gamma = 0$



$$Z_1 = \frac{1}{j\omega C_1}$$

$$Z_2 = \frac{1}{j\omega C_2}$$

① $\lambda_x = -g_m V_{gs}$

~~scribbled out text~~

② $V_x + V_{gs} = V_g$

③ $V_g = \lambda_x Z_2$

②+③ $\Rightarrow V_x + V_{gs} = \lambda_x Z_2$ ④

④+① $\Rightarrow V_x - \frac{\lambda_x}{g_m} = \lambda_x Z_2$

$\Rightarrow V_x = \lambda_x \left(\frac{1}{g_m} + Z_2 \right)$

$Z_{IN} = \frac{V_x}{\lambda_x} = \frac{1}{g_m} + Z_2 = \frac{1}{g_m} + \frac{1}{j\omega C_2}$

22-141 50 SHEETS
22-142 100 SHEETS
22-144 200 SHEETS
SAMPAD