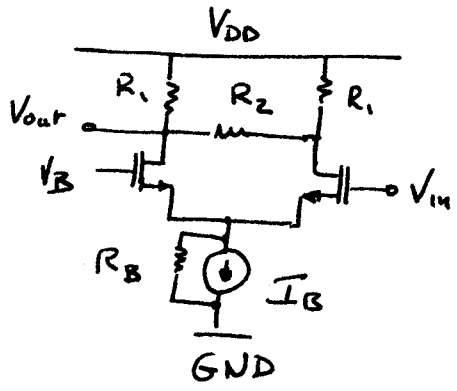


HOMEWORK # 4 SOLUTION

1)

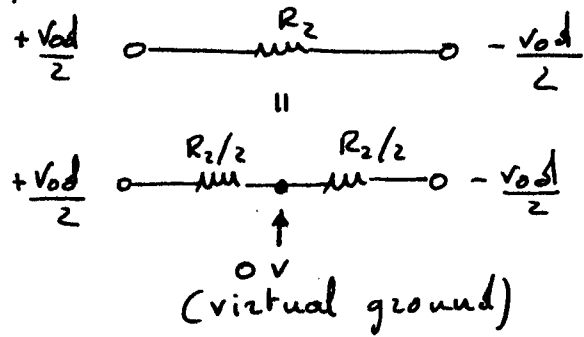
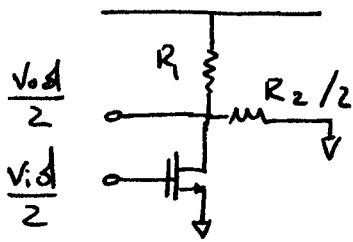


We will decompose the circuit into a differential mode half-circuit and a common mode half-circuit.

Let the subscripts 1 refer to the left side of the circuit and the subscripts 2 to the right side of the circuit.

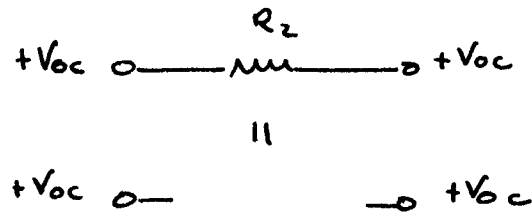
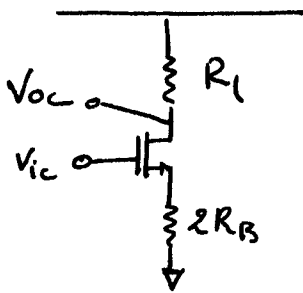
$$\begin{cases} v_{i1} = 0 \\ v_{i2} = v_{in} \end{cases} \Rightarrow \begin{cases} v_{ic} = (v_{i1} + v_{i2})/2 = v_{in}/2 \\ v_{id} = v_{i1} - v_{i2} = -v_{in} \end{cases}$$

differential-mode half-circuit



$$A_{dm} = -g_m (r_o \parallel R_1 \parallel \frac{R_2}{2})$$

common-mode half-circuit



$$A_{cm} = - \frac{g_m (r_o \parallel R_1)}{1 + g_m 2R_B}$$

total gain

$$\begin{aligned}v_{out} &= v_{o1} \\&= v_{oc} + v_{od} / 2 \\&= A_{cm} v_{ic} + A_{dm} v_{id} / 2 \\&= - \frac{g_m (r_o \parallel R_1)}{1 + 2g_m R_B} \frac{v_{in}}{2} \\&\quad - g_m (r_o \parallel R_1 \parallel \frac{R_2}{2}) (-v_{in}) / 2 \\&= \frac{g_m}{2} \left[r_o \parallel R_1 \parallel \frac{R_2}{2} - \frac{r_o \parallel R_1}{1 + 2g_m R_B} \right]\end{aligned}$$

$$A = \frac{v_{out}}{v_{in}}$$

$$\Rightarrow A = \frac{g_m}{2} \left[r_o \parallel R_1 \parallel \frac{R_2}{2} - \frac{r_o \parallel R_1}{1 + 2g_m R_B} \right]$$

$$2) \quad k' = \mu_0 C_{ox} = \mu_0 \frac{\epsilon_0 \epsilon_r \epsilon_{SiO_2}}{t_{ox}}$$

$$k'_{NMOS} = 250 \frac{cm^2}{Vs} \frac{8.85 \cdot 10^{-12} F/m \cdot 3.9}{2.6 \mu m}$$

$$= 250 \frac{cm^2}{Vs} \cdot 13.3 \text{ fF}/\mu m^2$$

$$= 332 \mu A/V^2$$

$$k'_{NMOS} \frac{W}{L_{eff}} = k'_{NMOS} \frac{W}{L-2LD} = 332 \frac{\mu A}{V^2} \frac{4 \mu m}{0.13 \mu m - 0.05 \mu m}$$

$$= 16.6 \text{ mA}/V^2$$

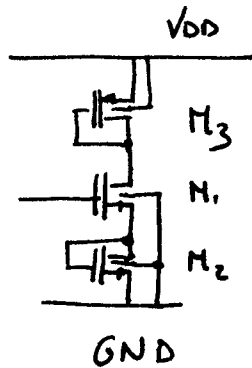
$$k'_{PMOS} = 100 \frac{cm^2}{Vs} \cdot 13.3 \text{ fF}/\mu m^2$$

$$= 133 \mu A/V^2$$

$$k'_{PMOS} \frac{W}{L_{eff}} = k'_{PMOS} \frac{W}{L-2LD} = 133 \frac{\mu A}{V^2} \frac{4 \mu m}{0.13 \mu m - 0.05 \mu m}$$

$$= 6.64 \text{ mA}/V^2$$

Large-signal analysis



$$\cdot \overline{I_{DS1}} = \overline{I_{DS2}} = |\overline{I_{DS3}}| = 150 \mu\text{A}$$

- Assume that M_1 is in saturation

$$\cdot \overline{I_{DS2}} = \frac{k'_n}{2} \frac{W}{L_{\text{eff}}} (V_{GS2} - V_{T0})^2 (1 + \lambda V_{GS2})$$

$$(\text{since } V_{GS2} = V_{DS2})$$

We will solve this equation iteratively:

$$V_{GS2} = V_{T0} + \sqrt{\frac{\overline{I_{DS2}}}{\frac{k'_n}{2} \frac{W}{L_{\text{eff}}} (1 + \lambda V_{GS2})}}$$

We start with an initial guess for V_{GS2} , fill this in in the right hand side of the equation and we get another value for V_{GS2} ; and so on... This iterative process should converge to an accurate enough estimate after a couple of iterations

$$V_{GS2} = 0 \rightarrow V_{GS2} = 434 \text{ mV} \rightarrow V_{GS2} = 429 \text{ mV}$$

$$\rightarrow \boxed{V_{GS2} = 429 \text{ mV}} \quad (\text{two iterations would have been enough})$$

$$\cdot |V_{GS_3} - V_{T0}| = \sqrt{\frac{|I_{DS_3}|}{\frac{\mu'}{2} \frac{W}{L_{eff}} (1 + \lambda |V_{GS_3}|)}}$$

$$|V_{GS_3}| = 0V \rightarrow |V_{GS_3}| = 513 \text{ mV} \rightarrow \boxed{|V_{GS_3}| = 505 \text{ mV}}$$

$$\cdot V_{SB_1} = V_{GS_2} = 429 \text{ mV}$$

$$\hookrightarrow V_{T_1} = V_{T0} + \gamma (\sqrt{2\phi_f + V_{SB_1}} - \sqrt{2\phi_f})$$

$$= 348 \text{ mV}$$

$$V_{DS_1} = V_{DD} - V_{GS_2} - |V_{GS_3}|$$

$$= 1.2V - 429 \text{ mV} - 505 \text{ mV}$$

$$= 266 \text{ mV}$$

$$V_{GS_1} = V_{T_1} + \sqrt{\frac{I_{DS_1}}{\frac{\mu'}{2} \frac{W}{L_{eff}} (1 + \lambda V_{DS_1})}} = 348 \text{ mV} + 131 \text{ mV}$$

$$= 479 \text{ mV}$$

(notice that $V_{GS_1} - V_{T_1} = 131 \text{ mV} < V_{DS_1} = 266 \text{ mV}$
so that M_1 is in fact in saturation
and our assumptions are self-consistent

$$V_{IN} = V_{GS_2} + V_{GS_1} = 429 \text{ mV} + 479 \text{ mV}$$

$$\Rightarrow \boxed{V_{IN} = 908 \text{ mV}}$$

Small-signal analysis

$$\begin{aligned} \textcircled{a} \quad R_{out} &= \frac{1}{g_{m3}} \parallel \left[\frac{1}{g_{m2}} + r_{o1} + r_{o2} \frac{g_{m1} + g_{m1} b_1}{g_{m2}} \right] \parallel r_{o3} \\ &\approx \frac{1}{g_{m3}} \parallel 2r_{o1} \parallel r_{o3} \\ &\approx \frac{1}{g_{m3}} \end{aligned}$$

$$\frac{1}{g_{m3}} = \frac{V_{Dsat3}}{2I_{D3}} = \frac{205\text{mV}}{300\mu\text{A}} = 683\Omega$$

$$\Rightarrow \boxed{R_{out} \approx 683\Omega} \quad \text{SPICE: } 667\Omega$$

$$\left(\frac{1}{g_{m3}} \parallel 2r_{o1} \parallel r_{o3} = 666\Omega \right)$$

$$a_v = \frac{-g_{m1}}{1 + \frac{g_{m1}(1+x_1)}{g_{m2}}} \cdot \frac{1}{g_{m3}} \quad (= +G_m \cdot R_{out})$$

$$\frac{g_{m1}(1+x_1)}{g_{m2}} \approx 1$$

$$\Rightarrow a_v = - \frac{V_{Dsat3}/V_{Dsat1}}{2}$$

$$\Rightarrow \boxed{a_v = -0.782} \quad \text{SPICE: } -0.734$$

$$\textcircled{b} \quad R_{out} = \frac{1}{g_{m2}} \parallel \frac{r_{o1} + 1/g_{m3}}{1 + g_{m1}(1+x_1)r_{o1}}$$

$$\approx \frac{1}{g_{m2}} \parallel \frac{1}{g_{m1}(1+x_1)}$$

$$x_1 = \frac{r}{2\sqrt{2\phi_f + V_{SB}}} = \frac{0.2 \text{ V}^{1/2}}{2\sqrt{600 \text{ mV} + 429 \text{ mV}}} = 0.1$$

$$\Rightarrow \boxed{R_{out} \approx 206 \Omega}$$

SPICE : 206 Ω

$$a_v = g_{m1} R_{out} = g_{m1} \left(\frac{1}{g_{m2}} \parallel \frac{1}{g_{m1}(1+x_1)} \right)$$

$$= \frac{1}{1+x_1} \parallel \frac{g_{m1}}{g_{m2}}$$

$$= \frac{1}{1+x_1} \parallel \frac{V_{Dsat2}}{V_{Dsat1}}$$

$$\times \frac{1}{2+x_1}$$

$$\Rightarrow \boxed{a_v \approx 0.476}$$

SPICE : 0.463

SPICE deck for problem 2a:

```
.title Homework 4 - Problem 2a

.option nomod post
.include ../models.sp

m1 out1 in out2 0 nmos w=4u l=0.13u
m2 out2 out2 0 0 nmos w=4u l=0.13u
m3 out1 out1 dd dd pmos w=4u l=0.13u

vdd dd 0 dc=1.2
vin in 0 dc=0.908 ac=1

.op
.tf v(out1) vin
.end
```

SPICE result for problem 2a:

```
***** operating point status is all simulation time is 0.
node =voltage node =voltage node =voltage
+0:dd = 1.2000 0:in = 908.0000m 0:out1 = 695.0375m
+0:out2 = 429.0277m
```

**** mosfets

```
subckt
element 0:m1 0:m2 0:m3
model 0:nmos 0:nmos 0:pmos
region Saturati Saturati Saturati
id 150.0512u 150.0512u -150.0512u
ibs -4.2903f 0. 0.
ibd -6.9504f -4.2903f 5.0496f
vgs 478.9723m 429.0277m -504.9625m
vds 266.0098m 429.0277m -504.9625m
vbs -429.0277m 0. 0.
vth 347.9627m 300.0000m -300.0000m
vdsat 131.0096m 129.0277m -204.9625m
beta 17.4849m 18.0262m 7.1437m
gam eff 200.0000m 200.0000m 200.0000m
gm 2.2907m 2.3259m 1.4642m
gds 28.4943u 27.6387u 20.9229u
gmb 225.8149u 300.2692u 189.0250u
```

**** small-signal transfer characteristics

```
v(out1)/vin = -734.3052m
input resistance at vin = 1.000e+20
output resistance at v(out1) = 667.2029
```

SPICE deck for problem 2b:

```
.title Homework 4 - Problem 2b

.option nomod post
.include ../models.sp

m1 out1 in out2 0 nmos w=4u l=0.13u
m2 out2 out2 0 0 nmos w=4u l=0.13u
m3 out1 out1 dd dd pmos w=4u l=0.13u

vdd dd 0 dc=1.2
vin in 0 dc=0.908 ac=1

.op
.tf v(out2) vin
.end
```

SPICE result for problem 2b:

```
***** operating point status is all simulation time is 0.
node      =voltage      node      =voltage      node      =voltage
+0:dd     = 1.2000  0:in      = 908.0000m 0:out1     = 695.0375m
+0:out2   = 429.0277m
```

**** mosfets

```
subckt
element  0:m1      0:m2      0:m3
model    0:nmos    0:nmos    0:pmos
region   Saturati Saturati Saturati
id       150.0512u 150.0512u -150.0512u
ibs      -4.2903f  0.         0.
ibd      -6.9504f  -4.2903f   5.0496f
vgs      478.9723m 429.0277m -504.9625m
vds      266.0098m 429.0277m -504.9625m
vbs      -429.0277m 0.         0.
vth      347.9627m 300.0000m -300.0000m
vdsat    131.0096m 129.0277m -204.9625m
beta     17.4849m  18.0262m  7.1437m
gam eff  200.0000m 200.0000m 200.0000m
gm       2.2907m   2.3259m   1.4642m
gds     28.4943u  27.6387u  20.9229u
gmb     225.8149u 300.2692u 189.0250u
```

**** small-signal transfer characteristics

```
v(out2)/vin          = 463.3582m
input resistance at  vin          = 1.000e+20
output resistance at v(out2)     = 206.1600
```